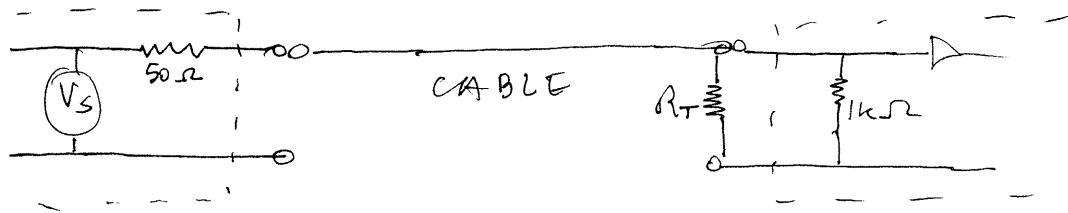


6b-4 -



d) Since we're dealing with fast pulses, we have to choose a cable and a termination that would match the input and output impedances, and thus eliminate signal reflections.

To obtain $50\ \Omega$ impedance we need a shunt resistor R_T of:

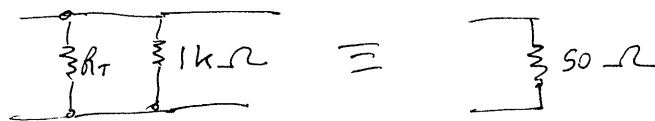
$$\frac{1}{50\ \Omega} = \frac{1}{R_T} + \frac{1}{1000\ \Omega} \Rightarrow R_T = \frac{50000}{950}\ \Omega = 52.6\ \Omega$$

The attenuation in decibels is:

$$A(\text{dB}) = 10 \log_{10} \left(\frac{P_{\text{out}}}{P_{\text{in}}} \right) \Rightarrow P_{\text{out}} = P_{\text{in}} \cdot 10^{\frac{A(\text{dB})}{10}}$$

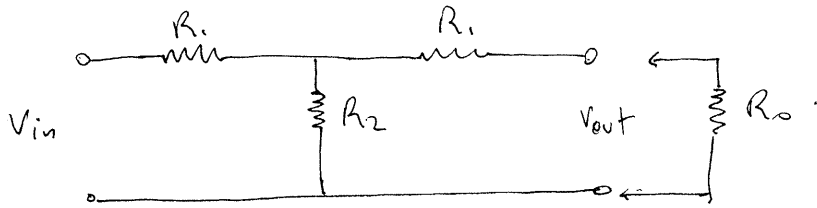
Thus a good cable is RG-178/U, which has $50\ \Omega$ characteristic impedance, and the largest attenuation value for the fast frequencies (400 MHz).

b)



$$\Rightarrow V_{\text{out}} = V_{\text{in}} = 5\text{V}$$

16.5



R_o - input and output impedances

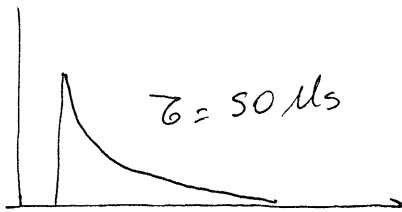
$$R_1 = R_o \frac{\alpha - 1}{\alpha + 1} ; R_2 = R_o \frac{2\alpha}{\alpha^2 - 1}$$

$$\alpha = \text{gain} = 10 ; R_o = 50 \Omega$$

$$R_1 = 50 \Omega \left(\frac{9}{11} \right) = \boxed{40.9 \Omega = R_1}$$

$$R_2 = 50 \Omega \left(\frac{20}{99} \right) = \boxed{10.1 \Omega = R_2}$$

16.7



$$V(t) = V_0 e^{-t/\tau}$$

$$\frac{V(t)}{V(0)} = 0.01 = \frac{e^{-t/\tau}}{e^0} = e^{-t/\tau}$$

$$t = -\tau \ln(0.01) = 50 \mu\text{s} (4.60517) \approx \boxed{230 \mu\text{s}}$$

16.8

In[2]:= Assuming[$\tau > 0 \ \&\& \ A > 0 \ \&\& \ k > 0$, DSolve[$\tau x'[t] + x[t] == A + (1 - e^{-\frac{t}{\tau}})$, x[t], t]]

Out[2]= {{x[t] $\rightarrow A e^{t(-\frac{1}{\tau} + \frac{1}{\tau}) - \frac{t}{\tau}} \left(e^{\frac{t}{\tau}} + \frac{k}{-k + \tau} \right) + e^{-\frac{t}{\tau}} C[1]}$ } $V_{out}(t) = E \left(1 + \frac{k}{\tau - k} e^{-t/k} \right) + C e^{-t/\tau}$

initial conditions:

$$V_{in}(0) = 0 = V_{out}(0) = E \left(1 + \frac{k}{\tau - k} \right) + C$$

$$\Rightarrow C = -E \left(\frac{\tau - k + k}{\tau - k} \right) = \frac{\tau E}{k - \tau}$$

$$\Rightarrow V_{out}(t) = E \left(1 + \frac{k}{\tau - k} e^{-t/k} + \frac{\tau}{k - \tau} e^{-t/\tau} \right)$$

$$\begin{aligned} \frac{dV_{out}(t)}{dt} &= E \left(\left(\frac{-1}{k} \right) \frac{k}{\tau - k} e^{-t/k} + \left(\frac{-1}{\tau} \right) \frac{\tau}{k - \tau} e^{-t/\tau} \right) \\ &= \frac{E}{\tau - k} \left(e^{-t/\tau} - e^{-t/k} \right) \end{aligned}$$

Plugging the results back into the diff. equation 16.17:

$$\begin{aligned} \tau \frac{dV_{out}}{dt} + V_{out} &= \frac{E \tau}{\tau - k} \left(e^{-t/\tau} - e^{-t/k} \right) + E \left(1 + \frac{k}{\tau - k} e^{-t/k} + \frac{\tau}{k - \tau} e^{-t/\tau} \right) \\ &= E e^{-t/k} \left(e^{t/k} + \frac{k}{\tau - k} - \frac{\tau}{\tau - k} \right) \\ &= E e^{-t/k} \left(e^{t/k} + \frac{k - \tau}{\tau - k} \right) = E \left(1 - e^{-t/k} \right) = V_{in} \quad \checkmark \end{aligned}$$

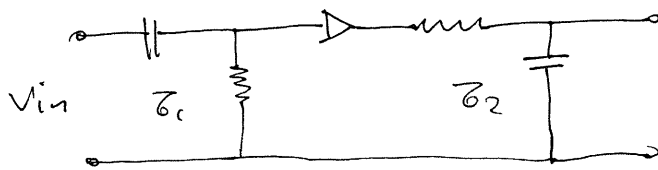
Limits $\rightarrow k \gg \tau$ low frequency signal

$$\Rightarrow \frac{\tau}{k - \tau} \sim 0 \Rightarrow V_{out}(t) = E \left(1 - e^{-t/k} \right) \approx V_{in}(t) \quad \checkmark$$

$$\rightarrow \tau \gg k \Rightarrow \frac{k}{\tau - k} \sim 0$$

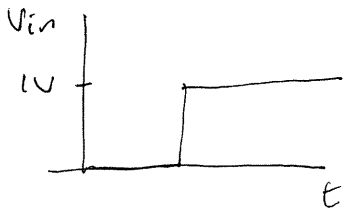
$$V_{out}(t) = E \left(1 - e^{-t/\tau} \right) - \text{response to a step function (16.21)} \quad \checkmark$$

16.10



CR-RC

$$\tau_1 = \tau_2 = \tau$$



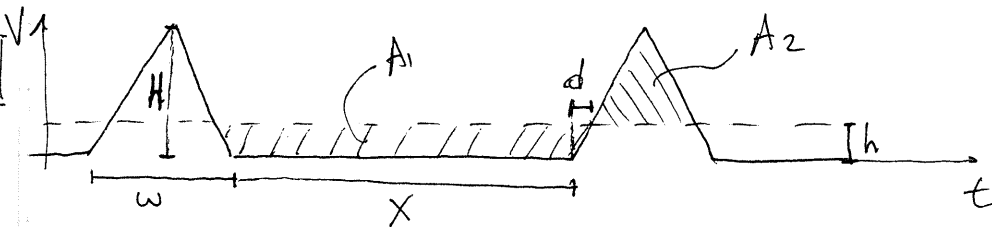
$$V_{out} = V_{in} \frac{t}{\tau} e^{-t/\tau}$$

$$\frac{dV_{out}}{dt} = V_{in} \left(\frac{e^{-t/\tau}}{\tau} - \frac{t}{\tau^2} e^{-t/\tau} \right) = \frac{V_{in}}{\tau} e^{-t/\tau} \left(1 - \frac{t}{\tau} \right)$$

$$\frac{dV_{out}}{dt} = 0 \Rightarrow 1 - \frac{t}{\tau} = 0 \Rightarrow t = \tau \text{ is a maximum for } V_{out}.$$

$$\frac{V_{out \max}}{V_{in}} = \frac{V_{out \max}}{1V} = \frac{\tau}{\tau} e^{-\tau/\tau} \Rightarrow V_{out \max} = \frac{1}{e} V \approx \boxed{0.368 V}$$

16.14



In steady state $A_1 = A_2$ (equal areas)

~~$A_1 = Xh$~~

$$A_1 = (X + d)h =$$

$$A_2 = \frac{1}{2} (H - h)(w - 2d)$$

$$H = 10V; w = 5\mu s.$$

and we also have $\frac{d}{h} = \frac{1}{2} \frac{w}{H} = \frac{1}{4} \frac{\mu s}{V}$

$$\Rightarrow \left(X + \frac{h}{4} \right) h = \frac{1}{2} (10 - h) \left(5 - \frac{h}{2} \right)$$

$$Xh + \frac{h^2}{4} = 25 - 5h + \frac{h^2}{4}$$

$$\Rightarrow (X + 5 \mu s) h = 25 \mu s \cdot V \cdot \mu s$$

$$\text{rate} = 100 \text{ s}^{-1} \Rightarrow T = \text{rate}^{-1} = 10000 \mu s = X + 5 \mu s$$

$$\text{baseline shift} = h = \frac{25 \mu s \cdot V}{10000 \mu s} = \boxed{2.5 \text{ mV}}$$

$$\text{rate} = 50000 \text{ s}^{-1} \Rightarrow X + 5 \mu s = \text{rate}^{-1} = 20 \mu s$$

$$\text{baseline shift} = \frac{25 \mu s \cdot V}{20 \mu s} = \boxed{1.25 \text{ V}}$$

16.15 The result of single delay line shaping is the superposition of the input pulse with a signal generated by its reflection in the coaxial cable. The reflection is inverted and delayed by twice the cable length.

signal velocity in RG-59/U cable = $0.659 c$

$$\Rightarrow \text{delay} = \frac{2 \times 10 \text{ m}}{3 \times 10^8 \text{ m/s} \cdot 0.659} \approx 101 \text{ ns}$$

