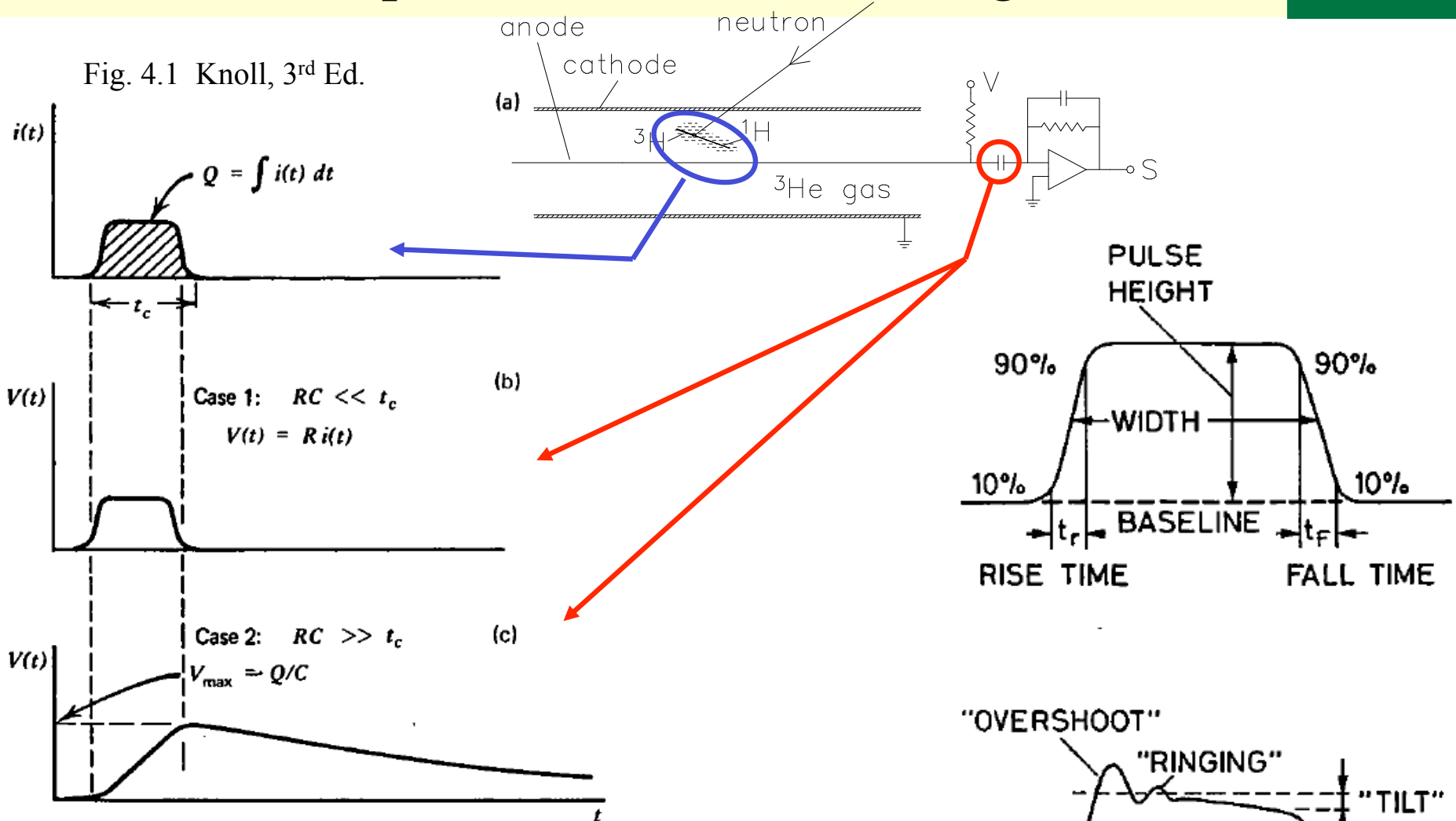


# Chap. 16a – Pulse Processing

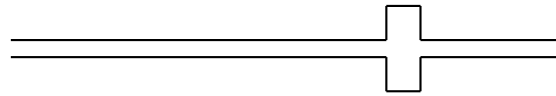


Leading or Falling edge  
 Rise or Fall time – 10:90%  
 (Uni or Bipolar // Analog or Digital)

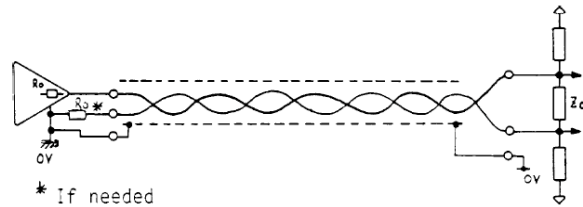
Fig. 11.1 Leo, 2<sup>nd</sup> Ed.

# Pulse Processing: cables

Twisted pairs – “differential” signals, logic or analogue

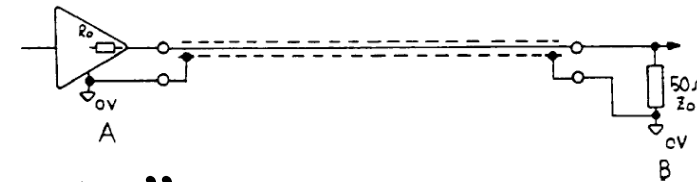


Shielded Twisted Pair Cable True Differential Input



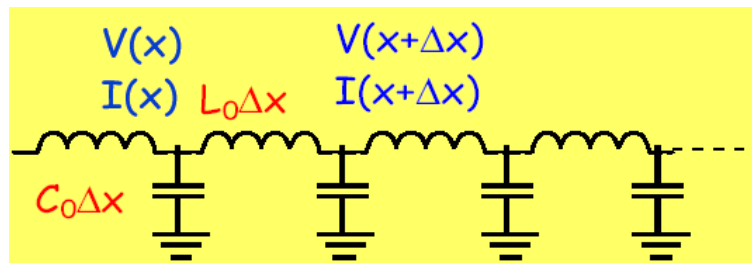
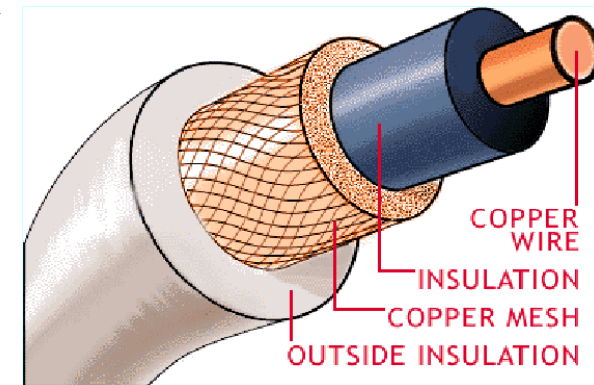
\* If needed

Coaxial Cable - Single-Ended Connection



Coaxial conductor/shield – signal on the “center”

Each configuration has a RG/U name with a characteristic capacitance and inductance per unit length, and an impedance (with a negligible resistance).



$$\frac{d^2V}{dx^2} = -\omega^2 L_0 C_0 V$$

$$V = Ae^{jkx} + Be^{-jkx} \quad k^2 = \omega^2 L_0 C_0$$

$$v = \frac{\omega}{k} = \frac{1}{\sqrt{L_0 C_0}}$$

$$Z_0 = \sqrt{\frac{L_0}{C_0}}$$

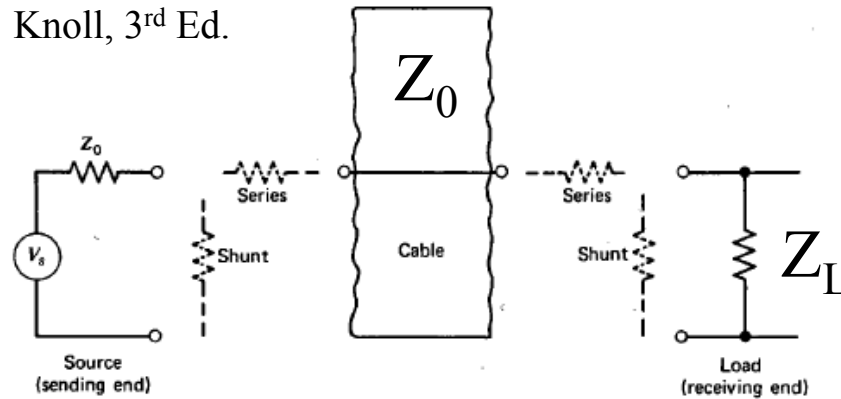
for coax

$$C_0 = 2\pi\epsilon / \ln(r_2 / r_1)$$

$$L_0 = (\mu / 2\pi) \ln(r_2 / r_1)$$

# Pulse Processing: impedance matching

Fig. 16.4 Knoll, 3<sup>rd</sup> Ed.



$$I_{Inc} + I_{refl} = I_L$$

$$V_{Inc} + V_{refl} = V_L$$

$$V_{refl} = -I_{refl} Z_0$$

$$\rightarrow \frac{V_{refl}}{V_{Inc}} = \frac{Z_L - Z_0}{Z_L + Z_0} \quad \& \quad \frac{V_L}{V_{Inc}} = \frac{2Z_L}{Z_L + Z_0}$$

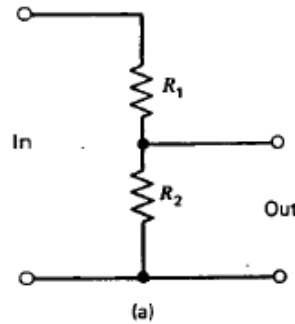
What happens?

- Open circuit ..  $Z_L \sim \infty$
- Short circuit ..  $Z_L = 0$
- Match circuit ..  $Z_L = Z_0$

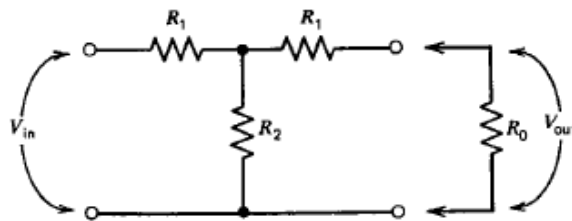
Match to get maximum transmission to load (S/N), minimize reflections (ringing), maintain signal shape.

Don't Match to minimize transmission .. Weak signals into high impedance loads or low power sources (but must use short cables).

# Pulse Processing: simplest manipulations



Voltage divider (recall PMT base)



$$\text{Attenuation } \alpha = V_{\text{out}}/V_{\text{in}}$$

$$R_1 = R_0 \frac{\alpha - 1}{\alpha + 1}$$

$$R_2 = R_0 \frac{2\alpha}{\alpha^2 - 1}$$

Fig. 16.5 Knoll, 3<sup>rd</sup> Ed.

Signal splitter:  $R = R_0/3$

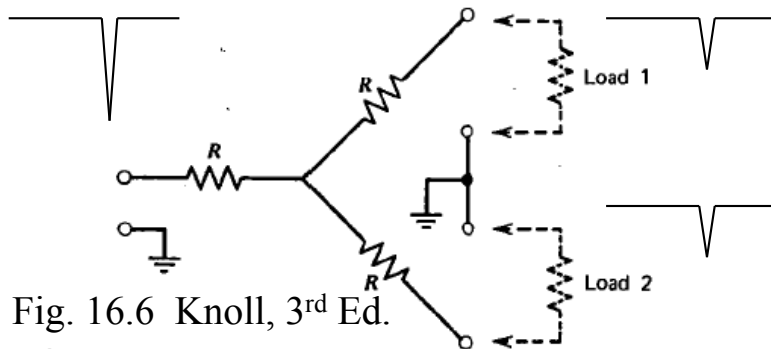


Fig. 16.6 Knoll, 3<sup>rd</sup> Ed.

Signal Inverter

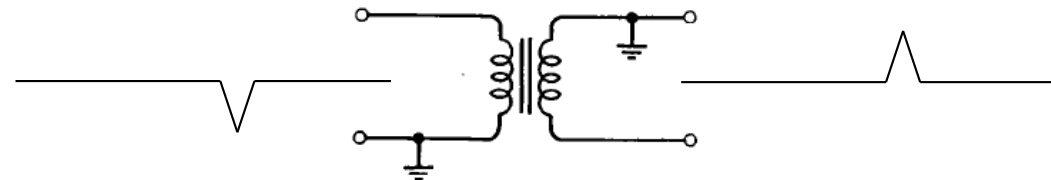
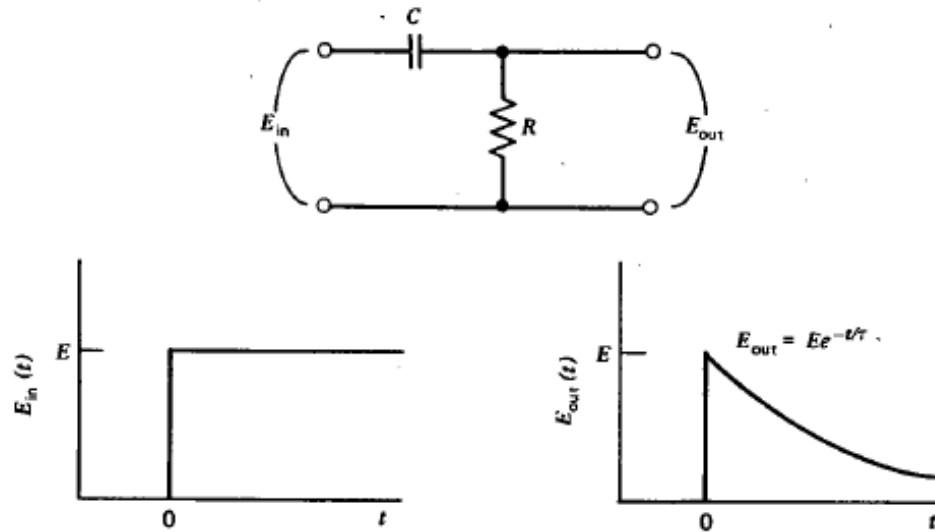


Fig. 16.7 Knoll, 3<sup>rd</sup> Ed.

All loads must be present, or else see previous discussion about reflections!

# Pulse Processing: CR circuit

Fig. 16.9 Knoll, 3<sup>rd</sup> Ed.



$$V_{in} = \frac{Q}{C} + V_{out}$$

$$\frac{dV_{in}}{dt} = \frac{1}{C} \frac{dQ}{dt} + \frac{dV_{out}}{dt} \quad (C \text{ is constant})$$

$$\frac{dV_{in}}{dt} = \frac{V_{out}}{RC} + \frac{dV_{out}}{dt} \quad dQ/dt = i = V/R$$

$$\tau \frac{dV_{in}}{dt} = V_{out} + \tau \frac{dV_{out}}{dt} \quad \tau = RC$$

$$V_{out} \approx \tau \frac{dV_{in}}{dt} \quad \text{for small } \tau$$

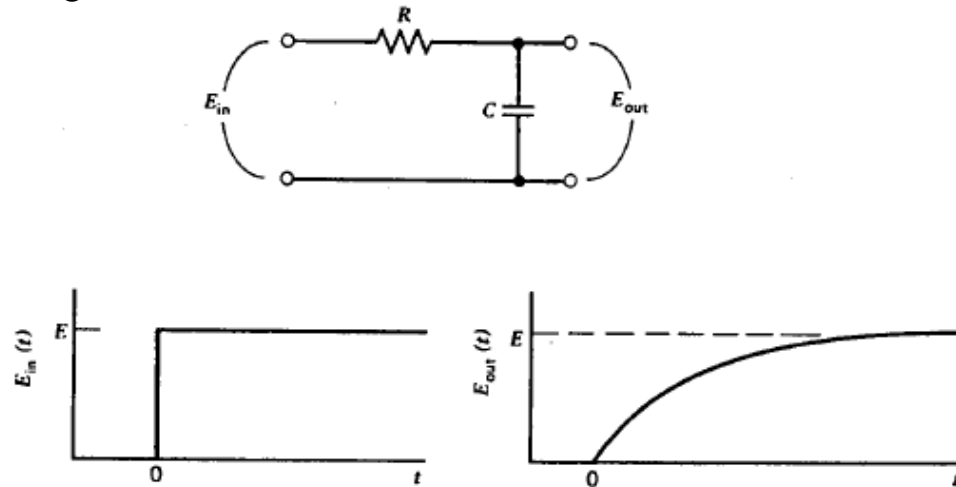
$$\tau \frac{dV_{out}}{dt} \approx \tau \frac{dV_{in}}{dt} \quad \text{for large } \tau$$

$$V_{out} \approx V_{in} \quad \text{"slow electronics"}$$

The differentiator (when  $\tau$  is small, “fast” electronics)  
 .. Should remove low frequency components and is called a “high-pass” filter.

# Pulse Processing: RC circuit

Fig. 16.10 Knoll, 3<sup>rd</sup> Ed.



$$V_{in} = iR + V_{out}$$

$$i = \frac{dQ}{dt} = C \frac{dV_{out}}{dt} \quad (\text{on capacitor})$$

$$V_{in} = RC \frac{dV_{out}}{dt} + V_{out}$$

$$\frac{V_{in}}{\tau} = \frac{dV_{out}}{dt} + \frac{V_{out}}{\tau}$$

$$\frac{V_{in}}{\tau} \approx \frac{dV_{out}}{dt} \rightarrow \frac{1}{\tau} \int V_{in} dt \approx V_{out}$$

$$V_{out} \approx V_{in} \quad \text{for small RC}$$

The integrator (when  $\tau$  is large, “slow” electronics)  
 .. Should remove high frequency components and is  
 called a “low-pass” filter.

# Pulse Processing: Cable Consequences

$$v = \frac{\omega}{k} = \frac{1}{\sqrt{L_0 C_0}}$$

$$Z_0 = \sqrt{\frac{L_0}{C_0}} \quad \text{so that} \quad Z_0 C_0 = \sqrt{L_0 C_0} = \tau$$

However, this is an unusual time constant – note that it has dimensions of (s / length )

The  $\tau$  depends on the length of the cable.

Some (poor) examples from Beldin Cables:

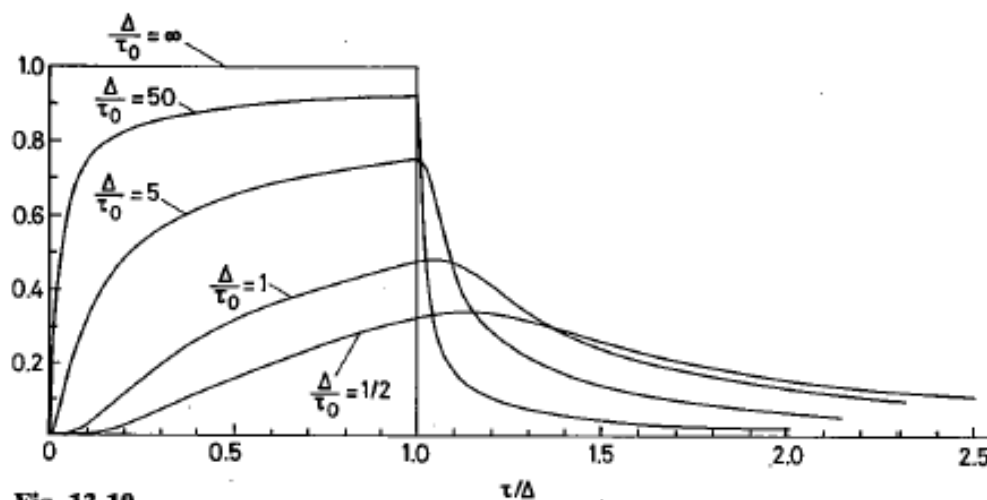
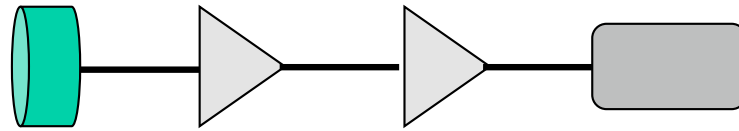


Fig. 13.10

Fig. 13.10 Leo, 2<sup>nd</sup> Ed.

	58 /U	59 /U	316 /U
$Z_0$	50 $\Omega$	75	50
$C_0$	24.3 pF/ft	16.3	29
$L_0$	0.064 $\mu$ H/ft	0.107	0.067
$v/c$	0.77	0.83	0.695
$\tau$	1.2 ns/ft	1.3 ns/ft	1.4 ns/ft

# Pulse Processing: Question



Electronics in the vault or not?

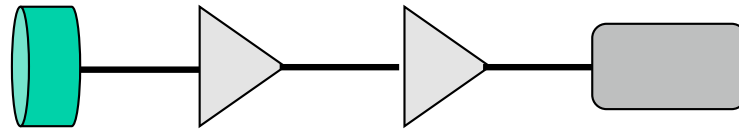


Compare the output of a preamp step-function pulse that passes through a 1m Beldin RG-58/U cable to that that passing through 50 m of the same cable. Use the Fermi function with  $a=1\text{ns}$  ,  $t_0=10$ , and  $t$  in ns.

$$f(t) = 1/(1 + e^{-(t-t_0)/a})$$



# Pulse Processing: Answer



Electronics in the vault or not?



Compare the output of a preamp step-function pulse that passes through a 1m Beldin RG-58/U cable to that that passing through 50 m of the same cable. Use the Fermi function with  $a=1\text{ns}$ ,  $t_0=10$ , and  $t$  in ns.

